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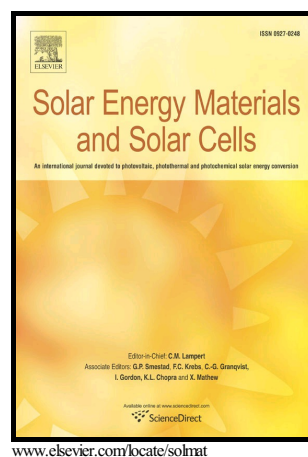
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Advanced characterisation and optical simulation for the design of solar selective coatings based on carbon: transition metal carbide nanocomposites

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Abstract

Solar selective coatings based on carbon transition metal carbide nanocomposite absorber layers were designed. Pulsed filtered cathodic arc was used for depositing amorphous carbon: metal carbide (a-C:MeC, Me = V, Mo) thin films. Composition and structure of the samples were characterized by ion beam analysis, X-ray diffraction, Raman spectroscopy, and transmission electron microscopy. The optical properties were determined by ellipsometry and spectrophotometry. Three effective medium approximations (EMA), namely Maxwell-Garnett, Bruggeman, and Bergman, were applied to simulate the optical behaviour of the nanocomposite thin films. Excellent agreement was achieved between simulated and measured reflectance spectra in the entire wavelength range by using the Bergman approach, where in-depth knowledge of the nanocomposite thin film microstructure is included. The reflectance is shown to be a function of the metal carbide volume fraction and its degree of percolation, but not dependent on whether the nanocomposite microstructure is homogeneous or a self-organized multilayer. Solar selective coatings based on an optimized a-C:MeC absorber layer were designed exhibiting a maximum solar absorptance of 96% and a low thermal emittance of ~5 and 15% at 25 and 600°C, respectively. The results of this study can be considered as a predictive design tool for nanomaterial-based optical coatings in general.

Keywords

Solar selective coatings; Amorphous carbon: transition metal carbides; Effective Medium approximation; Pulsed filtered cathodic vacuum arc; Bergman representation

1 Introduction

Concentrating solar power (CSP) is a commercially available technology in the field of renewable energies. It is based on the conversion of concentrated solar energy into thermal and subsequently electrical energy. Nowadays, the two most prominent commercial CSP technologies are parabolic trough collectors and central receiver tower plants. Main

components of CSP technology are solar light concentrators (reflectors), solar receivers (absorbers), heat transport and storage systems and electrical power generators [1]. Solar selective coatings with high absorptance (α) in the solar spectral range (0.3 – 2.5 μm) and low thermal emittance (ε_T) in the infrared region (2.5 – 30 μm) are required for solar receivers [2]. Physical vapor deposited (PVD) solar selective coatings have been widely employed in parabolic trough systems, where temperatures below 400 °C and vacuum environments are applied [3]. However, these solutions cannot be directly implemented in central receiver tower plants that operate at higher temperatures in air. Nowadays, commercial paints such as Pyromark® are the most commonly employed absorber coatings in tower plant central receivers. Their disadvantages are a poor solar selectivity ($\varepsilon = 86\%$ at room temperature) and a fast degradation during operation. The latter one requires permanent maintenance and repairs typically every two years [4]. In a recent review [3], an extensive variety of PVD coatings was evaluated. Correspondingly, the coatings degrade easily at high temperatures ($>400^\circ\text{C}$) in air due to oxidation and/or diffusion of the metal substrate into the coatings. These examples underline the necessity to develop novel types of solar selective coatings that are characterized by high-temperature stability in oxidizing environments.

State of the art designs of solar selective coatings include multilayers comprised of an antireflective layer (AR), an absorber layer, and an infrared reflection (IR) layer. Antireflective layers such as a Si_3N_4 or Al_2O_3 located on the top of the coating improve the solar absorption and stabilize the coating at high temperatures [5]. The infrared reflective layer placed under the absorber layer reduces the thermal emittance at high temperatures and acts as a thermal barrier to avoid material diffusion between the absorber material and the substrate [6].

Solar absorber layers based on nanocomposite materials were investigated in numerous studies [7,8]. Among them, a-C:MeC nanocomposites are suitable candidates for high-temperature solar absorber applications [9]. Pure a-C thin films are good candidates for solar absorber materials [10] but they are not air stable at temperatures above 300°C. In combination with group 4, 5, and 6 transition metals, carbon forms a number of exceptionally stable interstitial carbides. These carbides are characterized by high melting points (in the range of 2600-2800°C [11]), high thermal and electrical conductivity, and high reflectivity in the entire UV-Vis-IR spectral range [12]. The presence of these carbides stabilizes the nanocomposite microstructure at high temperatures [13,14]. Different microstructures of the a-C:MeC nanocomposites have been reported i) carbide phases dispersed in the carbon matrix in the form of nanoparticles, with different morphologies (globular or elongated [15,16]) and

crystal structures (amorphous [17] or crystalline [18]) and ii) a self-forming multilayer structure with periodic concentration fluctuations of metal in a-C [19]. These systems can exhibit improved mechanical properties (lower intrinsic compressive stress, improved adherence to the substrate or better wear resistance [20]) compared to pure a-C films.

Combining the advantageous optical and thermo-mechanical properties of the individual components can result in adjustable solar selective properties for a-C:MeC nanocomposites with high-temperature resistance. Harding et al. reported that sputter deposited metal carbides (Cr, Fe, Mo, Ni, Ta and W) on copper substrates show good selective properties ($\alpha > 80\%$ and $\mathcal{E}_{600^\circ\text{C}} \sim 7\%$) [21,22]. Gampp developed a multilayer coating based on hydrogenated a-C co-deposited with Cr or W by sputtering (a-C:H/Cr and a-C:H/W [23–25]). Yin et al. [26] deposited a-C:H/SS-a-C:H (SS: stainless steel) using cathodic arc technique. However, in all these examples the optical properties dropped drastically for temperatures higher than 600°C due to different types of degradation mechanisms: i) undesired interaction between coatings and the metallic bottom layer and ii) degradation due to the intrinsic instability of the coating material itself. More recently, Schüller et al. developed a multilayer coating based on titanium and amorphous hydrogenated carbon (a-C:H/Ti) films [27] adding silicon to increase the durability in air.

The proper determination of the optical constants of the nanocomposites represents a major difficulty for the optimization of a-C:MeC solar absorber coatings up to now. This is particularly caused by the limited knowledge on the dependences of optical properties in the solar range on nanocomposite film composition, microstructure and phase morphology. In heterogeneous materials with nanoparticles much smaller than the light wavelength (such as a-C:MeC thin films), the optical properties can be described by so-called effective dielectric functions or effective medium approximations (EMA) [28]. They give a non-trivial average of the dielectric functions of the individual components of the nanocomposite in the form of an effective dielectric function (ϵ_{eff}) for the composite material.

Several EMAs have been established, Maxwell-Garnett (MG) [29] and Bruggeman (BRU) being the most widely used ones [30]. In both, the final effective dielectric function depends on the volume fraction of the particle material and on the optical constants of the individual constituents. Characteristic properties of the microstructure or the shape of the embedded particles are not incorporated. In contrast, Bergman (BER) representation [31] applies several corrections related to the shape of the nanoparticles and the degree of percolation of the embedded nanoparticles, which improve the accuracy of the simulated effective dielectric

function. This approximation is especially useful in cases where the microstructure plays a significant role in the optical properties of the heterogeneous material.

By now the design of absorber coatings relies very often on an empirical *ad-hoc* approach. A smart coating development, however, would require a reliable simulation of the optimized coating stack as the first and the experimental confirmation as the second step. The former would have to identify and incorporate those structure elements that are relevant for the optical response. Therefore, the first objective of this study is to apply such approach to model the optical properties of a-C:VC and a-C:MoC nanocomposite films as a solar absorber layer. The second objective is to design a complete solar selective AR layer / a-C:MeC absorber layer / IR reflector stack by using this model and to find out the theoretical limit of the absorbance at RT and at temperatures relevant for high-temperature absorber applications.

In this study, a-C:VC and a-C:MoC nanocomposite thin films with different metal carbide contents and different microstructures have been deposited by pulsed filtered cathodic vacuum arc (PFCVA). Among the different physical vapour deposition (PVD) techniques, FCVA has the highest plasma ionization ratio. This results in denser thin films with higher hardness and better adhesion [32], and allows the control of the composition ratio of absorbing carbon and reflecting/refractory carbide. The element composition of the nanocomposites was determined using Rutherford Backscattering Spectrometry (RBS) and Nuclear Reaction Analysis (NRA). Their structure was characterized by Raman spectroscopy, X-ray diffraction (XRD), and high-resolution transmission electron microscopy (HRTEM). Reflectance spectra were obtained by UV-Vis-NIR spectrophotometry, and the optical constants were measured by spectroscopic ellipsometry (SE). The optical properties were simulated comparing three different EMAs, namely Maxwell Garnett, Bruggeman and Bergman using the commercial software CODE [33]. The Bergman EMA was found to be the most suitable one for this type of materials. The dielectric functions obtained by the simulation were further used for a detailed examination of the absorptance of a-C:MeC (Me = V, Mo) layers. Based on this approach an optimized, complete stack with an outstanding solar absorptance (α) of 96% and an emittance (ε_T) of 5/15% at 25/600°C was predicted. This is significantly better than the values reported for this class of materials so far, which were an $\alpha=91.0\%$ with $\varepsilon_{100^\circ\text{C}} = 11\%$ for an a-C:TiC/SiO₂ stack on Cu substrate [27,34].

2.1 Thin film growth

Thin films were simultaneously grown on single crystalline Si (100) and on polished Inconel® 625 substrates in the same deposition batches. The former ones were used for Rutherford Backscattering Spectroscopy (RBS), Raman and XRD characterization while the latter were employed for high-resolution transmission electron microscopy (HRTEM) and optical characterization. Before deposition, the substrates were cleaned in an ultrasonic bath in distilled water, acetone and ethanol.

The depositions were carried out using a PFCVA system equipped with two arc sources, PFCVA-450 from Plasma Technology Limited [35] (Figure 1). The system includes electromagnetic filters in the curved ducts to reduce the incorporation of macroparticles in the growing films. The generated arc plasmas are guided into the vacuum chamber by an electromagnetic field applied to the curved ducts. External solenoid coils are wrapped around the ducts and produce an axial magnetic field. The coils are biased with 20 V and a current of 15 A to build up a lateral electrical field.

The substrates were situated on a rotating holder in the center of the chamber, 240 mm away from the exit of the duct. A negative pulse bias voltage of -400 V (100 kHz, 20% duty cycle) was applied to the substrates during film deposition in order to improve adhesion and to release the residual stress of the coating [36]. The sample holder was rotated with a continuous rotation speed of 1.4 rpm. The deposition chamber was evacuated to a pressure of $2 \cdot 10^{-3}$ Pa before deposition. During film deposition, an argon flow of 3.5 sccm was introduced into the chamber to stabilize the arc, and the working pressure was kept constant at 0.11 Pa by a pressure control valve.

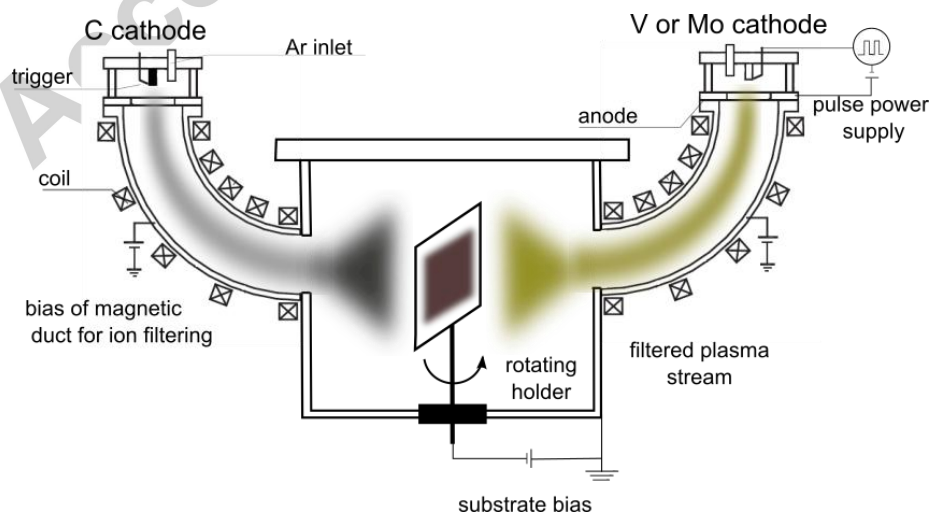


Figure 1: Schematic diagram of the pulsed filtered cathodic vacuum arc (PFCVA) system equipped with two cathodic arc sources.

One arc source is used as carbon cathode and the other as a metallic one (vanadium or molybdenum). a-C:MeC coatings were prepared by simultaneous co-evaporation of both cathodic arc sources. The discharge pulse duration was 3 ms at a repetition rate of 7.5 Hz, with adjustable intensity. The deposition time was 30 minutes. All the deposition parameters are summarized in Table 1.

Table 1: Deposition parameters of the C and a-C:MeC thin films deposited with PFCVA. All the samples were deposited at room temperature on Si (100) and Inconel substrates

Parameter	Value
Base pressure (Pa)	$2.00 \cdot 10^{-3}$
Working pressure (Pa)	0.11
Argon flow (sccm)	3.5
Deposition time for a-C:MeC samples (min)	30
Deposition time for C (min)	60
Duct bias (V)	-20
Duct current (A)	15
Axial magnetic field (G)	200
Cathodes	99.997% C 99.993% V 99.995% Mo
Cathode diameter (mm)	10
Discharge current for carbon (A)	2.5
Discharge current for high/ low metal content (A)	5 / 1.25
Pulse duration [frequency] of the discharge (ms) [Hz]	3 [(7.5)]
Bias voltage at deposition stage (V)	- 400 (100 kHz pulsed)
Duty cycle of the bias (%)	20
Rotation speed of the substrate (rpm)	1.4
Filter to the substrate distance (mm)	240

Both carbon – vanadium carbide (a-C:VC) and carbon – molybdenum carbide (a-C:MoC) thin films were deposited with two different metal concentrations, denoted as high (h) and low (l) throughout this article. The metal concentration was controlled via the cathode current ratio R , given by $R = I_{\text{carbon}} / I_{\text{metal}}$. Therefore, the carbon arc source current was kept constant and the metal arc source current was varied in such a way that R was either 0.5 for high metal content samples and 2.0 for low metal content ones.

A pure carbon reference film was prepared by applying the same deposition conditions expect of using only the carbon arc source and extending the deposition time to 60 minutes.

2.2 Thin films microstructure characterization

The carbon and metal (V or Mo) areal densities of films grown on Si substrates were determined by a combination of Rutherford Backscattering Spectroscopy (RBS) and Nuclear Reaction Analysis (NRA) measurements. The RBS intensity of scattered deuterium ions is proportional to the atomic number Z of all elements of the sample. Here it was used for the determination of the metal contents. Since the RBS cross section of carbon is low and the

carbon signal is superimposed to that of the Si substrate. NRA measurements were employed to accurately determine carbon areal densities.

The RBS and NRA measurements were carried out at a 2 MeV Van der Graff and a 3 MeV Tandem accelerator, respectively. The RBS spectra were obtained by using ^4He ions with energy of 1.7 MeV. The data were acquired with a silicon barrier detector located at a backscattering angle of 170° , whose energy resolution was 13 keV. The simulation software SIMNRA [30] version 6.06 was used to extract the metal areal density. NRA was measured by using 1.248 MeV deuterium ions as incident particles at a detection angle of 135° . The nuclear reaction $^{12}\text{C}(d,p)^{13}\text{C}$ has its maximum cross section at an incident deuterium ion energy of around 1.248 MeV. The intensity of the emitted proton radiation is proportional to the carbon concentration in the nanocomposite thin film [37]. The carbon content was determined quantitatively by integrating the NRA intensity and comparing it with that of a C:Ni reference sample.

The thickness and roughness of the deposited samples were measured using a 50x objective Confocal Microscope (Plμ 2300, SENSOFAR).

The phase structure of the carbon matrix was determined by Raman spectroscopy. Micro-Raman spectra were recorded on a LabramHR spectrometer (Horiba, Germany), which is equipped with a liquid N_2 cooled charge-coupled device detector and coupled to a BH2 microscope (Olympus, Germany). The laser beam of a Nd:YAG solid-state laser with a wavelength of 532 nm was focussed to a spot diameter of 1 μm using a 50-fold magnifying objective. The laser power at the sample was 1mW. The scattered light was collected in an 180° backscattering geometry and dispersed by a 300 line/mm grating. No sample degradation occurred under these conditions. For the analysis of the Raman line shape, the software PeakFit (version 4.12, Seasolve Software Inc.) was employed. The measured spectra were fitted with a combination of a linear background fixed at the noise level of the spectra at 850 - 2000 cm^{-1} , a symmetric Lorentzian shape for the *D*-peak, and an asymmetric Breit-Wigner-Fano (BWF) line for the *G*-peak [13,38,39]. The intensity I as a function of the wavenumber ω for the BWF line shape is described by equation (1):

$$I(\omega) = \frac{I_0[1+2(\omega-\omega_0)/q\Gamma]^2}{1+[2(\omega-\omega_0)/\Gamma]^2} \quad (1)$$

with the intensity maximum (I_{max})

$$I_{max} = I_0 [1 + 1/q^2] \quad (2)$$

positioned at

$$\omega_{max} = \omega_0 + \Gamma/2q, \quad (3)$$

where I_0 is the peak intensity, ω_0 the peak position, Γ the FWHM, and q is the BWF coupling coefficient. The intensity maximum defined by equation (2) will be used to denote the intensity of the G and D peaks and equation (3) to define their wave number.

The phase structure of the dispersed phase in the a-C:MeC thin films was determined by X-ray diffraction employing grazing incidence geometry (GIXD) using a PANalytical X'Pert PRO diffractometer with Cu- K_α radiation ($\lambda=1.5406$ Å). The incident angle was 0.4° , and the XRD patterns were measured in the diffraction angle range of $30\text{--}100^\circ$ in steps of 0.05° . The crystallite size of the main crystal directions was estimated employing the Scherrer equation with k of 0.94 [40].

The microstructure was analysed by cross-sectional HRTEM with a TECNAI F30 microscope operated at 300kV accelerating voltage. It is equipped with Schottky-type field emission gun and an ultra-high resolution pole piece. The thin lamellas required for the cross-section analysis were made using a Focused Ion Beam (FIB) Dual Beam Helios 650, consisting of a 30kV Ga focused ion beam combined with a 30kV electron beam placed at 52° between them, and with the Omniprobe® manipulator. Sample-protecting Pt thin films were deposited by electron beam deposition of $(\text{CH}_3)_3(\text{C}_p\text{CH}_3)\text{Pt}$.

2.3 Determination of optical properties

The specular reflectance at room temperature was measured in the range 250 to 3300 nm using a Shimadzu UV-Vis-NIR Solid Spec-3700 spectrophotometer under an incident angle of 5° from the normal. The system is equipped with three detectors (PMT, PbS and InGaAs) which ensure sufficient sensitivity in the whole wavelength range. An aluminum mirror was used as a reference and the reflectance was corrected by using a calibrated Al standard. The software CODE was employed to simulate the reflectance spectra.

Based on the reflectance spectrum, the solar absorptance (α), defined as the fraction of incident radiation in the solar wavelength range that is absorbed, is calculated according to equation (4) [41]:

$$\alpha = \frac{\int_{\lambda_1}^{\lambda_2} [1-R(\lambda)]G(\lambda)d\lambda}{\int_{\lambda_1}^{\lambda_2} G(\lambda)d\lambda} \quad (4)$$

where $\lambda_1 = 300$ nm and $\lambda_2 = 2500$ nm denote the integration limits, $R(\lambda)$ the spectral reflectance, and $G(\lambda)$ is the reference solar spectrum AM 1.5. The thermal emittance is calculated applying Kirchoff's law from the reflectance spectra in the infrared region, following equation (5):

$$\varepsilon(T) = \frac{\int_{\lambda_1}^{\lambda_2} [1-R(\lambda,T)]B(\lambda,T)d\lambda}{\int_{\lambda_1}^{\lambda_2} B(\lambda,T)d\lambda}, \quad (5)$$

where $B(\lambda, T)$ is the spectral distribution of the blackbody radiation calculated with Plank's law [42] for a specific temperature T in Kelvin degrees. The integration interval is limited by $\lambda_1 = 1 \mu\text{m}$ and $\lambda_2 = 25 \mu\text{m}$, based on European standard EN-673:2011 [43].

3 Results and discussion

3.1 Film composition, density and roughness

In order to calibrate the equivalent areal density for each metal content, data obtained in RBS experiments of samples with the highest vanadium and molybdenum content (a-C:VC (h) and a-C:MoC (h) samples) were used. The RBS spectra (Figure 2) show the V and Mo metal signals at approximately 1280 and 1480 keV, respectively. Due to the high Z of both metals, these signals are strong and clearly differentiated from the overlapping signals of the silicon substrate and carbon below 900 keV and at 440 keV, respectively. The weak peak around 1100 keV is caused by the incorporation of less than 3 at.% Ar used to stabilize the arc formation during the deposition. A closer look at the vanadium RBS signal in a-C:VC (h) (inset in Figure 2a) reveals an inhomogeneous depth distribution of the metal. In fact, in order to fit the spectrum properly, five different layers with alternating high (22 at.%) and low (17 at.%) vanadium content were taken into account. To a lesser extent, this depth inhomogeneity of the metal concentration is also observed in the a-C:MoC (h) nanocomposite. In this case, it was necessary to assume three different regions with 17, 25, and 14 at.% Mo to fit the RBS spectrum properly. These results will be discussed in detail later in combination with HRTEM images.

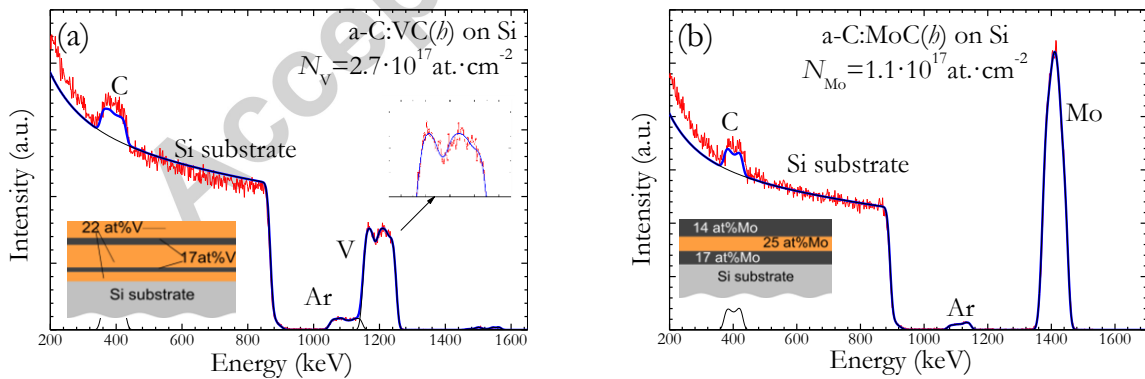


Figure 2: RBS spectra of (a) a-C:VC and (b) a-C:MoC thin films with high metal content, to calculate the equivalent metal concentration. The modulation of the composition in the a-C:VC samples is represented in the inset of (a).

The nuclear reaction of the carbon atoms with deuterium ions gives rise to the proton signal at approximately 3100 keV [54], while the backscattered deuterium ions contribute to the RBS part of the spectrum (Figure 3). At the measurement conditions, 1000 counts correspond to

$5.77 \cdot 10^{17}$ carbon atoms/ cm^2 , as determined from a reference C-Ni sample, and $2.7 \cdot 10^{17}$ and $1.1 \cdot 10^{17}$ atoms cm^{-2} for vanadium and molybdenum, respectively, extracted from RBS analysis. The total amount of carbon and metal atoms deposited per unit area (t_C and t_{Me} respectively) was determined by integrating the peak areas of the NRA and RBS signals for each sample and subsequent summation. The metal-carbon ratio in percent was calculated as shown in equation (6):

$$\text{at. \%}(Me) = \frac{t_{Me}}{t_{Me} + t_C} \times 100\%. \quad (6)$$

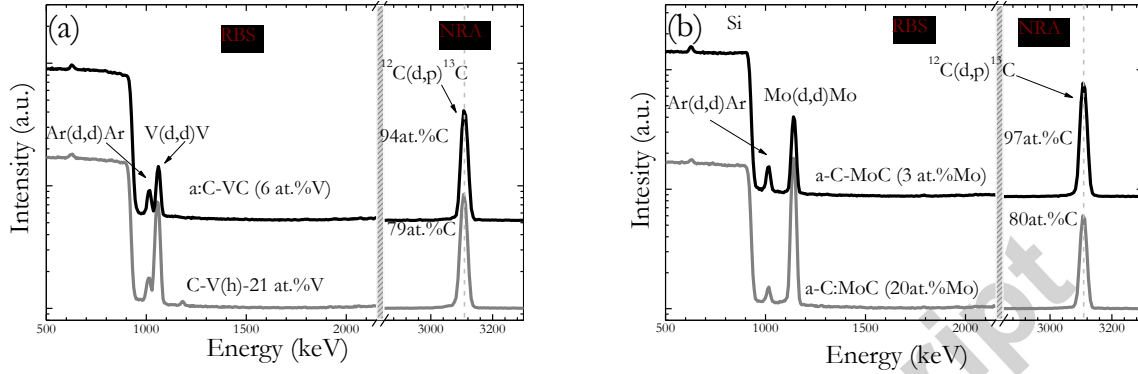


Figure 3: NRA spectra of (a) a-C:VC and (b) a-C:MoC for high and low metal content films. Two distinct regions in the spectra are indicated as RBS and NRA, corresponding to backscattered deuterium signal and nuclear reaction proton signal, respectively.

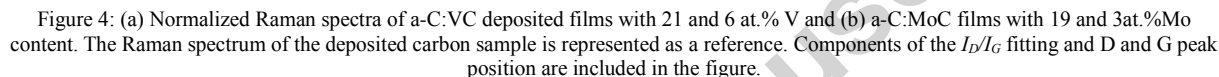
The averaged metal contents of the samples are given in Table 2. The film density can be estimated from the RBS areal density and film thickness [44]. In the case of a-C:VC (h) sample, the density is $\sim 3.0 \text{ g}\cdot\text{cm}^{-3}$, i.e. lower than the density of bulk vanadium carbide ($5.7 \text{ g}\cdot\text{cm}^{-3}$ [45]) and higher than in amorphous carbon ($2.1 \text{ g}\cdot\text{cm}^{-3}$ [46]) typically obtained with cathodic arc deposition. In the case of the a-C:MoC (h) sample, the estimated average density is 4.8 g cm^{-3} .

The thickness, deposition rate and roughness of the samples grown on silicon are summarized in Table 2. The deposition rate of samples deposited on Inconel was by a factor of 1.39 ± 0.03 nm/min higher than those on Si. It is worth noting that the average roughness (R_a) is below 3 nm for the films grown on Si substrates. This indicates the formation of ultra-smooth surfaces due to the effective removal of the macroparticles with the curved filters.

Table 2: Metal content, thickness, deposition rate and roughness of PFCVA deposited thin films on silicon substrates.

Sample	Metal content (at.%)	Thickness (nm)	Deposition rate (nm/min)	R_a (nm)
a-C:VC (high)	21 ± 1	140 ± 5	4.8 ± 0.2	2.5 ± 0.2
a-C:VC (low)	6 ± 1	110 ± 10	3.7 ± 0.2	2.7 ± 0.2
a-C:MoC (high)	19 ± 1	90 ± 15	3.0 ± 0.2	2.7 ± 0.2
a-C:MoC (low)	3 ± 1	125 ± 10	3.3 ± 0.2	2.8 ± 0.2
a-C	0	150 ± 5	2.5 ± 0.2	3.1 ± 0.2

The Raman spectra of the a-C:MeC nanocomposite films exhibit a shape that is constituted of a shoulder in the range of the *D*-line and a maximum at the Raman shift of the G line of sp^2 -C. The ratio of the peak intensities I_D/I_G increases with increasing metal content from 0.50 for a-C:MoC (3 at.% Mo) via 0.56 (6 at. % V) and 0.64 (19 at. % Mo) to 0.80 for a-C:VC (21 at.% V). The position of the G line is observed at 1540 to 1545 cm^{-1} for all samples. The three-stage model of Ferrari and Robertson [47] implies a sp^2 -C phase consisting of a-C with a higher degree of 6-fold aromatic ring clusters than in the reference sample of pure carbon. The corresponding sp^3 -C content of the carbon matrix in all the a-C:MeC samples is of the order of 10 to 15 %. The increasing I_D/I_G ratio reveals that the metal addition promotes formation of 6-fold aromatic rings in the amorphous carbon matrix of both a-C:MeC types [48] in comparison to pure carbon films.



3.3 Phase structure of the nanocomposites

agreement with the reference value (4.16 Å). Employing Scherrer equation with 0.94 as the value of the form factor K , a minimum crystal size of (27 ± 10) nm was estimated. The second set of interferences is observed at 2θ values of 36.7° , 42.7° , 63.0° , and 74.9° . The diffraction angles are slightly smaller than those of the first set, and moreover, the peaks are significantly broader. The diffractogram pattern points to a second *fcc*-VC structure with a lattice constant of 4.25 Å and a minimum crystal size of (7 ± 4) nm. The coexistence of two *fcc*-VC phases can be rationalized by assuming regions with a different V content, what is consistent with the observed fine structure of the RBS signal. The data are in qualitative agreement with those of a recent study on magnetron sputtered a-C:CV films [39]. Similar as in the present study, a slight decrease of the VC lattice constant with increasing V content was reported therein. Moreover, the minimum crystal size increased from (1.7 ± 0.2) nm for 19 at.% V to (6 ± 1) nm for 27.9 at.% V. No significant diffraction peaks were identified in the low metal content a-C:VC sample with 6 at. % V (Figure 5 a).

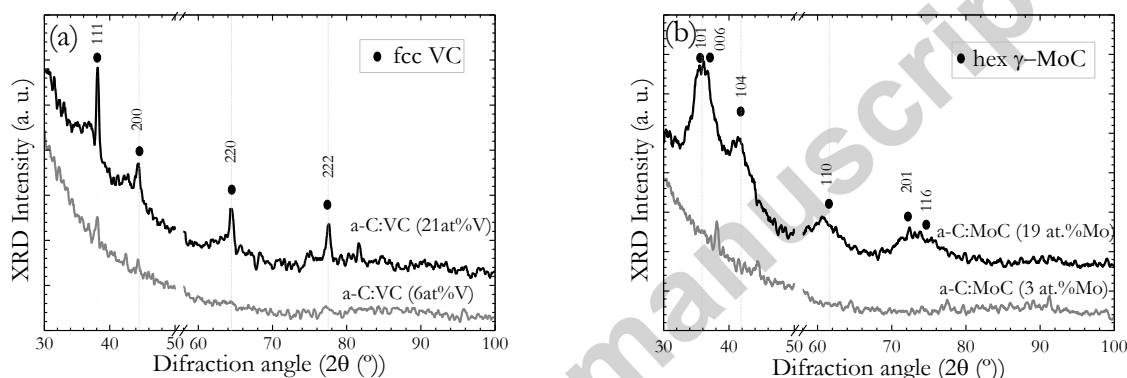


Figure 5: XRD patterns of (a) a-C:VC and (b) a-C:MoC for samples with high and low metal content. The dotted lines indicate the more significant peaks position of the referred crystal phases. The patterns are intercepted between ~ 50 and 58° in order to omit the intense Si (311) peak at $\sim 52^\circ$ of the Si (100) substrate

Figure 5b shows the XRD pattern of the a-C:MoC samples. The diffractogram of a-C:MoC (~ 19 at.% Mo) shows four broad diffraction peaks at $2\theta = 36^\circ$, 41° , 61° and 73° . The pattern closely resembles that of simple hexagonal monocarbide γ -MoC [49]. Its main peaks are tabulated at $2\theta = \sim 36^\circ$, 42° , 61° and 73° and assigned to the crystal planes (101), (104), (110) and (116), respectively. The main peaks observed here for a-C:MoC (~ 19 at.% Mo) are also close to those of *hcp* β -Mo₂C [49]. According to the binary phase diagram of Mo and C [51], the thermodynamically stable phase for a Mo content of ≤ 50 at.% is γ -MoC with hexagonal simple space group $P6m2$. Therefore we tentatively assign the observed diffractogram of a-C:MoC (19 at.% Mo) to the γ -MoC phase. The phase structure of a-C:MoC (19 at.% Mo) will be further discussed in the subsequent section about the HRTEM analysis. Scherrer equation gives a minimum γ -MoC crystallite size of 3.5 ± 0.5 nm.

For a-C:MoC (3 at.% Mo), no significant diffraction peaks were identified. As for a-C:VC (6 at.% V), the low metal content is presumably responsible for a small number of MeC crystals, which moreover are too small in order to provide a sufficiently large volume for coherent scattering of X-rays that is necessary for the observation of diffraction interferences.

In summary, only for high metal content films nanocrystalline carbides are observed. No crystalline phases can be identified for low metal content films. It seems that the excess of carbon limits the growth of crystalline carbide grains during deposition [52]. Neither crystalline metal nor graphitic phases are observed. The latter finding is in agreement with the Raman analysis.

3.4 Film morphology

A multilayer structure is observed for a-C:VC (21 at.% V) in the cross-sectional TEM images of Figure 6. In total, five regions are found. Three of them exhibit an ordered multilayer pattern with a period of (5 ± 1) nm. In the other two this periodicity is apparently lost (Figure 6a). The observed layer sequence is correlated with the different compositional ranges observed in RBS (see Figure 2). High-resolution imaging was applied for detailed analysis of the ordered and non-ordered regions of a-C:VC (21 at.% V) in Figure 6b. The two different regions are labeled as 1 and 2. The FFT analysis of the non-ordered region 1 reveals only one lattice plane distance of 2.4 Å (Figure 6c). This distance is attributed to the (111) planes of *fcc*-VC phase, revealing VC nanocrystals embedded in the a-C matrix.

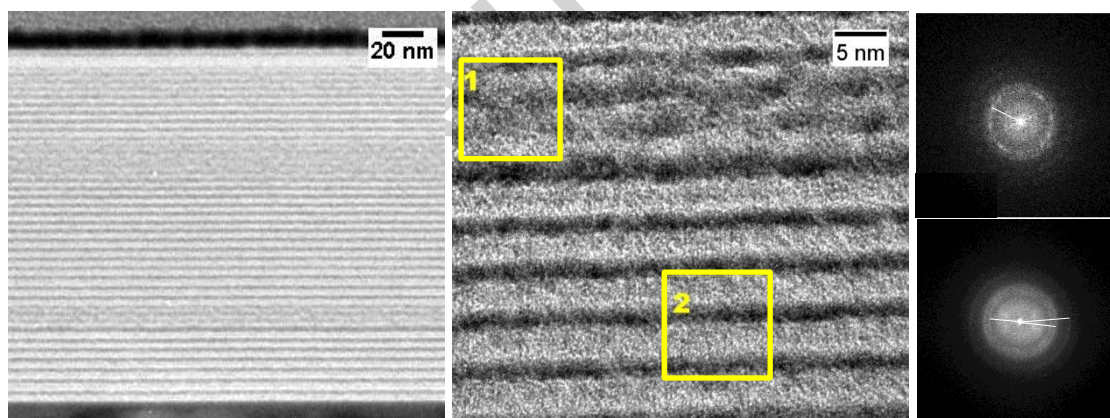


Figure 6: HRTEM analysis of a-C:VC (21 at.%V) deposited on Inconel. (a) Overview image, (b) high-resolution image of a representative sample section, (c) and (d) FFTs analysis of selected regions 1 and 2 of (b), respectively.

The self-organized multi-layers of region 2 are composed of alternating dark contrast carbide-rich (~ 1 -1.5 nm thick) and bright contrast carbide-depleted (~ 3 -4 nm) nanolayers. The FFT of this region shows three circular intensity maxima (Figure 6d). The corresponding lattice plane distances of 1.4, 2.0 and 2.4 Å are in very good agreement with those of *fcc*-VC [53].

The multilayer structure observed for a-C:VC (21 at.% V) cannot be associated with the sample rotation during the deposition process as the periodicity of the layers does not match the rotation speed of the substrate holder and the sample holder orientation has no effect on microstructure evolution. Moreover, it is not correlated with the pulse sequence during the deposition. Therefore, the formation of the layered structure is attributed to a self-organization process already reported in the literature [54–57].

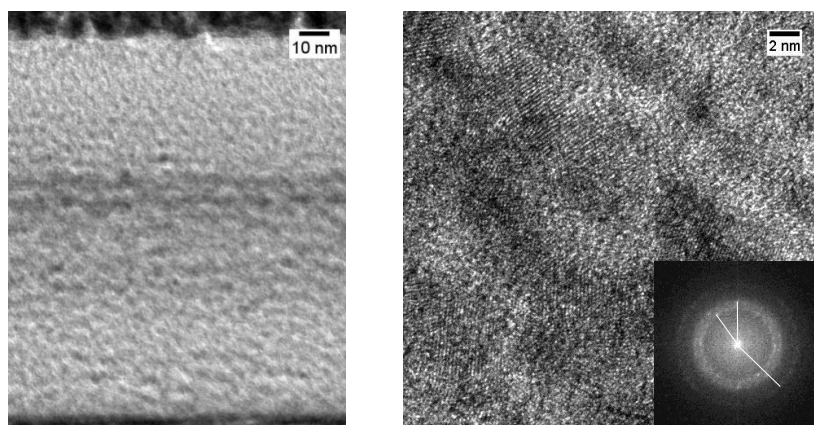


Figure 7: HRTEM analysis of a-C:MoC (19 at.%Mo) deposited on Inconel. (a) cross-section image, (b) high-resolution image of an illustrative sample area, with FFTs analysis of (b).

HRTEM images of the a-C:MoC (19 at.% Mo) sample (Figure 7a) reveal three different regions, two metal carbide depleted (brighter areas) and one metal carbide-rich (darker area). This is consistent with the three regions identified by RBS analysis (Figure 2).

High-resolution TEM images reveal molybdenum carbide nanoparticles embedded in a carbon matrix (Figure 7b). The FFT analysis gives three circular intensity maxima associated with lattice parameters of 1.5, 2.1 and 2.5 Å (inset Figure 7b). These interplanar distances are in good agreement with those of the (110), (103) and (101) crystal planes of γ -MoC. Based on the slightly better agreement of the lattice plane distances and the thermodynamics the carbide phase of this nanocomposite is attributed to γ -MoC and not to β -Mo₂C.

In summary, the comprehensive characterization gives a consistent scenario of the microstructure evolution of the nanocomposites under study. The formation of nanocomposites structures of dispersed metal carbide crystals embedded in amorphous carbon was confirmed by Raman, XRD and TEM for the samples with high metal content. The phase structure is thermodynamically driven by the immiscibility of the phases which lead to a phase separation. In addition to the generally observed phase separation, a spontaneous formation of ordered multilayers for the case of the a-C:VC (21 at.% V) thin film is found.

This complete microstructural characterization of the thin films will be applied for additional information required in the simulations of the optical properties in the following section. The variety of obtained microstructures and the comprehensive characterization provides the basis

for a complete simulation of the optical properties of the a-C:MeC nanocomposite solar absorber layers.

3.5 Optical properties of a-C:VC and a-C:MoC films

In order to simulate the optical properties of heterogeneous materials, it is crucial to find a proper EMA which accurately describes the combined effect of the nanocomposite components. Therefore, the measured reflectance spectrum of a selected nanocomposite film, namely a-C:VC (21 at.% V), was compared to simulated spectra obtained by using Maxwell-Garnett (MG) [47], Bruggeman (BRU) [48], and Bergman (BER) [49] models (Figure 8).

In the simulations, the amorphous carbon was considered to form the matrix material. The strong dependence of the a-C optical constants on the ion energy, the substrate temperature, the plasma density and the sp^3 fraction, make their correct estimation a complex issue. Hence, the optical constants of the a-C matrix were estimated from spectroscopic ellipsometry (SE) measurements performed on the a-C reference sample. For an a-C deposited with FCVA with sp^3 content ~20%, Ferrari et al [46] estimated a density of $2.1 \text{ g}\cdot\text{cm}^{-3}$.

No metallic phase was experimentally found in any of the single layers (see section 3.3 and 3.4). Therefore, the MeC was considered to be the particle component of the nanocomposite. The metal atomic percentage obtained experimentally by RBS-NRA was converted into volume fraction (VF) of metal carbide using the densities of the individual components. MeC optical constants and density values of 5.6 and $9.5 \text{ g}\cdot\text{cm}^{-3}$ for VC and γ -MoC were obtained from literature data [11,58,59].

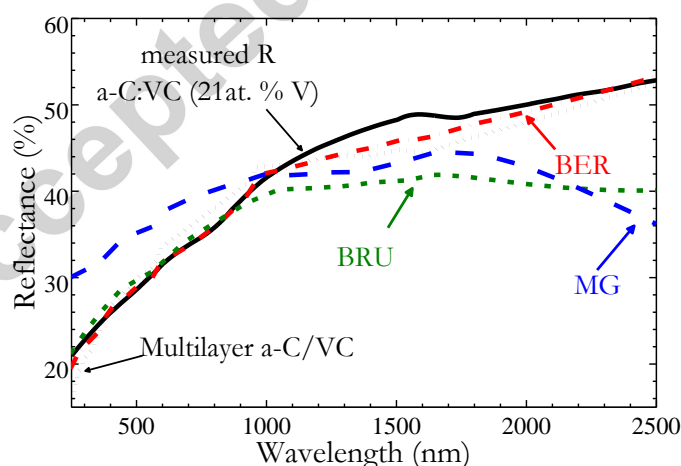


Figure 8: Comparison of measured reflectance spectrum of a-C:VC (21 at.%), (solid black line) with simulation data obtained for the same composition employing Maxwell-Garnett (MG), Bruggeman (BRU) and Bergman (BER) effective medium approximations, with the equivalent 41.3% volume fraction of VC, and 42 multilayer structure alternating between a-C (5nm) and VC (4nm) nanolayers.

The comparison of the simulated and measured spectra reveals that Bergman model properly describes the experimental reflectance of a-C:VC (21 at.% V) in the whole wavelength range

(Figure 8). These significant differences of the three EMAs are also reflected in the solar absorptance (Table 3).

Table 3: Solar absorptance of deposited a-C:VC (21at.% V) sample compared with the calculated solar absorptance for the equivalent simulated sample by Maxwell-Garnett, Bruggeman and Bergman EMA theories and with the multilayer a-C/VC.

EMA model	Solar absorptance (%)
Maxwell- Garnett (MG)	61.3 \pm 0.1
Bruggeman (BRU)	65.3 \pm 0.1
Bergman (BER)	63.8 \pm 0.1
Multilayer a-C / VC	63.7 \pm 0.1
Measured Reflectance $R(\lambda)$	64.3 \pm 0.1

Maxwell-Garnett overestimates the experimental reflectance by up to 10% in the visible and underestimates it by up to 15% in the near infrared spectral range, giving the largest deviation of the simulated α ($\Delta\alpha = -3.0\%$) from all the EMAs employed. MG approximation is only applicable to systems with volume fraction below 30% without percolation. As the volume fraction of the carbide particles in the a-C:VC (21 at.% V) is 41%, a high degree of percolation is expected, accounting for the strong deviation of MG simulation shown in Figure 8.

Bruggeman theory is adequate for large particle volume fraction and percolated systems. It is the most commonly used approximation as it only requires the particle volume fraction as simulation parameter. However, this approach does not properly simulate the experimental reflectance spectra for a-C:VC films. This model provided an excellent agreement for the visible range but underestimated the reflectance in the near-infrared range. This results in small deviation of solar absorptance ($\Delta\alpha = +1.0\%$), but from deviations in the IR range one could expect misleading thermal emittance values.

As mentioned above, Bergman gives the best agreement between the simulated and experimental spectra in the whole wavelength range, with the most accurate value of solar absorptance ($\Delta\alpha = -0.5\%$). A tentative explanation for this finding is that this EMA incorporates the shape and degree of percolation of the embedded nanoparticles as additional parameters to the simulation. BER formula is described in equation (7).

$$\varepsilon_{eff} = \varepsilon_M \left(1 - f \int_0^1 \frac{g(n,f)}{t-n} dn \right) \text{ with } t = \frac{\varepsilon_M}{\varepsilon_M - \varepsilon_P} \quad (7)$$

Where ε_p and ε_M are the particles and matrix material dielectric functions respectively, and ε_{eff} the effective dielectric function of the nanocomposite, t is a combined dielectric property (takes real values between 0 and 1), f is the particle volume fraction. $g(n,f)$ is a function called spectral density as expressed by equation (8):

$$g(n,f) = g_0(f)\delta(n) + g_{cont}(n,f) \quad (8)$$

Consequently, the fitting procedure involves three parameters: volume fraction, percolation strength, and n , an arbitrary number of points that are used to define the shape of $g(n,f)$ by a cubic spline interpolation. With the BER representation, the average dielectric functions ε_{eff} of the composite material were calculated from the individual components (ε_M and ε_P).

In order to clarify whether the multilayer structure of a-C:VC (21 at.% V) observed in the HRTEM images affects the optical film properties, a multilayered structure was also simulated. It is formed of 21 bilayers of pure metal carbide and pure amorphous carbon of 4 and 5 nm thickness, respectively, corresponding to the measured carbide volume fraction (41% VF). No significant differences were observed between the multilayer reflectance simulation ($\alpha=63.7\%$) and BER simulation as shown in Table 3. This result implies that the film growth mode (self-organized layered structure or dispersed carbide nanoparticles embedded in a-C matrix) does not affect the optical properties. A similar result has been observed in solar selective coatings based on silicon nitride cermets [60].

Once the appropriateness of the Bergman model to simulate a-C:MeC composites is demonstrated, this EMA was used to simulate reflectance spectra and solar absorptance for the all studied nanocomposite samples (Figure 9).

The function $g(n,f)$ cannot be computed analytically for real systems since the topology is too complicated or not even known. BER representation parameters were calculated by adjusting $g(n,f)$ to experimental data, and the fitting parameters are further detailed in the Table S2 of the supplementary data. The effective dielectric function obtained provides additional information related to the shape of the nanoparticles and their degree of percolation. BER theory is especially interesting when the microstructure plays a significant role in the optical properties of the heterogeneous material.[61]

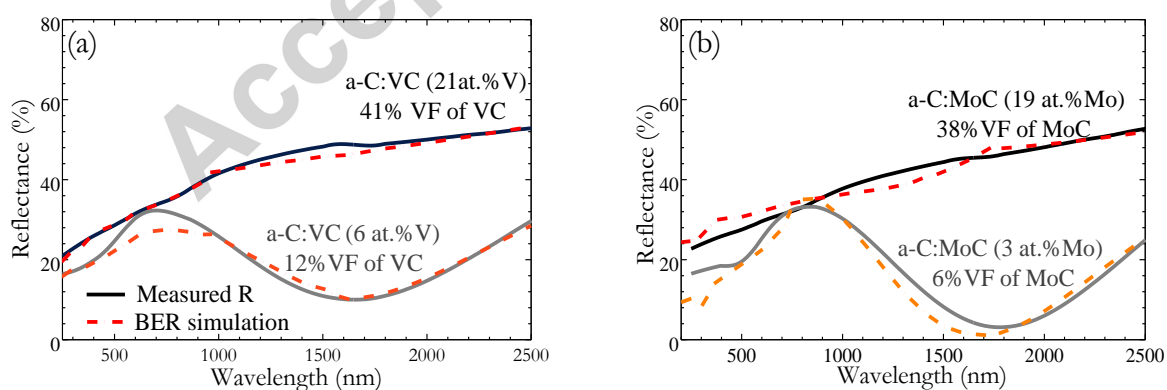


Figure 9: Comparison of measured and simulated reflectance spectra of (a) a-C:VC and (b) a-C:MoC for samples with higher and lower metal content. a-C:VC (21 at.% V) has been represented in Figure 8, but is plotted again here for comparison. Solid lines represent the measured reflectance spectra and the dash-dot is the simulated reflectance following Bergman EMA.

An excellent agreement was obtained for all the studied systems, independently of the metal carbide content. Bergman model allows extracting percolation behaviour according to the metal content in the samples. In the case of nanocomposites with higher metal content, the percolation strength (g_0) necessary to ensure a correct fit between measured and simulated spectra was ~ 1 . This is an indication of interconnection of the embedded carbide particles, pointing to a metallic character of the a-C:MeC(h) films. On the contrary, samples with low metal content, exhibit no percolation ($g_0(f)=0$). This is characteristic for a dielectric or insulating behaviour, caused by the missing connection between the carbide particles.

On the basis of the Bergman representation, the solar absorptance (α) was computed as a function of carbide volume fraction and thickness (Figure 10) for samples on Inconel substrate.

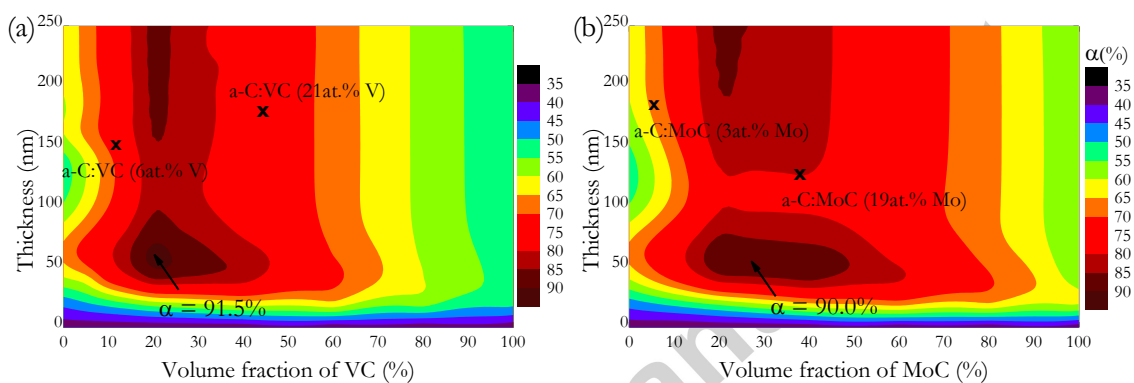


Figure 10: Solar absorptance for different thicknesses and volume fraction values of (a) a-C:VC and (b) a-C:MoC. The maximum absorptance for each a-C:MeC type obtained from simulation, as well as the experimentally deposited samples, are also included in the graphs.

In both systems, the absorptance maximum was found for a volume fraction in the range of 15 to 40% VF. By variation of the thickness, α increases from 36% (absorptance of the inconel substrate) until it reaches a maximum for a thickness of 50 to 70 nm. The maximum α is 91.5 ± 0.5 % for a 62 nm thick a-C:VC single layer with 19 % volume fraction of VC (equivalent to 9.7 at.% of V) on Inconel substrate. In the case of the a-C:MoC system, a maximum absorptance of 90 ± 0.5 % was found for a film with thickness of 55 nm and 28% VF of MoC (14 at.% Mo). For thicknesses higher than 150 nm, the absorptance increases again, reaching a maximum constant value similar to the one in the thinner range. However, increasing the absorber layer thickness can negatively affect to interlayer adherence and/or increase of thermal emittance in a complete solar selective coating. Hence, the thickness considered for further simulations was in the 50-70 nm range.

Using the knowledge gained from the individual absorber layer study, a complete solar selective stack structure (AR/a-C:MeC/IR) was simulated (Figure 11). Al_2O_3 with ~ 45 nm thickness was selected as AR layer due its high-temperature resistance and inertness in

relation to the environment. For the absorber layer, the optimized thickness and volume fraction values for a-C:VC and a-C:MoC were adopted. A 400 nm TiN infrared reflectance layer was also added between the substrate and the a-C:MeC in order to reduce the emittance in the infrared part of the spectrum.

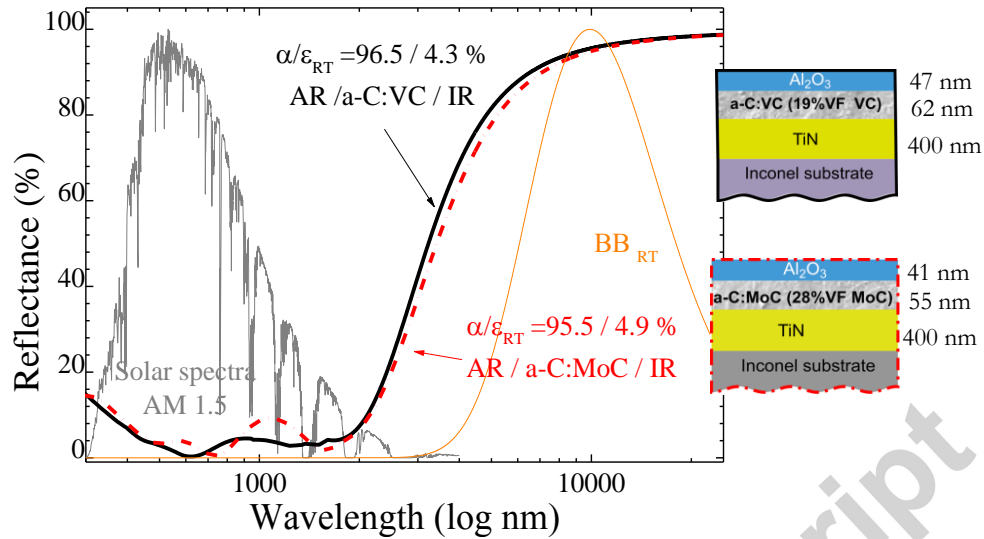


Figure 11: Simulated reflectance spectra of $\text{Al}_2\text{O}_3/\text{a-C:VC}$ (19%VF VC)/TiN and $\text{Al}_2\text{O}_3/\text{a-C:MoC}$ (28%VF MoC)/TiN of the optimized solar selective coatings. The solar spectrum (AM1.5) and the black body radiation at 25°C (Planck's law) are included.

The solar selective coatings for both the AR / a-C:VC / IR and AR / a-C:MoC / IR coatings, provide a selectivity ratio $\alpha/\epsilon_{RT} = 96.5/4.3$ at RT. At 600°C, the emittance increases up to 14% and 15% for the simulated a-C:VC and a-C:MoC based multilayer stack, respectively. Those values are among the best performing reported for simulated layer stacks using a-C:MeC ($\alpha = 91.0\%$ and $\epsilon_{100^\circ\text{C}} = 11\%$ for a-C:TiC/SiO₂ on Cu substrate) [27,34] as absorber layer. The optimized values for cermet as absorber were $\alpha = 95.0\%$ with $\epsilon_{300^\circ\text{C}}$ of 9% for a graded W-AlN [62,63].

4 Conclusions

Solar selective surfaces have been designed based on carbon transition metal carbide absorber layers. Filtered cathodic arc was used for depositing a-C:VC and a-C:MoC films. For higher metal content (~21 at.% V and ~19 at.% Mo) film microstructure consists of metal carbides particles embedded in an amorphous carbon matrix for samples deposited with higher metal content. In the case of a-C:VC films, a self-organized arrangement of multilayers was observed.

Reflectance spectra were simulated employing different EMA models using experimentally measured optical constants for a-C. An excellent agreement between simulated and measured reflectance for single a-C:MeC layers was only achieved in the whole wavelength range using

a Bergman approach. This approach requires a detailed microstructural analysis for an accurate optical simulation in inhomogeneous materials.

Using Bergman EMA model, the maximum solar absorptance of $91.5 \pm 0.5 \%$ is obtained for the a-C:VC single layer on Inconel substrate with a film 62 nm thickness and 19 % volume fraction of VC (equivalent to 9.7 at.% of V). In the case of the a-C:MoC system, it is possible to reach an absorptance of $90 \pm 0.5 \%$ for a film with thickness of 55 nm and 28% volume fraction of MoC (14 at.% of metal Mo).

The simulation of a complete solar selective surface and antireflective and IR mirror layers leads to a solar absorptance higher than 96% with a thermal emittance at room temperature below 5% and 15% at 600°C. This demonstrates the potential of a-C:MeC as an absorber layer material for high-temperature applications. Further experimental studies should be carried out on such solar selective surfaces in order to test the validity of the predictions of this study on optical properties at RT and high temperature as well as to test thermal and environmental stability.

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Highlights

- Solar selective surfaces have been designed based on carbon transition metal carbide absorber layers, deposited by pulsed filtered cathodic vacuum arc.
- Film microstructure consists of metal carbides particles embedded in an amorphous carbon matrix. Self-organized arrangement of multilayers was observed for a-C:VC films.
- An excellent agreement between simulated and measured reflectance was only achieved in the whole wavelength range using a Bergman approach, which requires a detailed microstructural analysis.
- A complete solar selective coating was simulated achieving solar absorptance higher than 96% and a thermal emittance at room temperature below 5% and 15% at 600°C.